

Control Systems Stability and Robust Control

Relative Degree and Zero Dynamics

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Example

- Consider the controlled van der Pol equation:

$$\dot{x}_1 = x_2/\varepsilon, \quad \dot{x}_2 = \varepsilon \left[-x_1 + x_2 - \frac{1}{3}x_2^3 + u \right], \quad y = x_1$$

$$\dot{y} = \dot{x}_1 = x_2/\varepsilon, \quad \ddot{y} = \dot{x}_2/\varepsilon = -x_1 + x_2 - \frac{1}{3}x_2^3 + u$$

Hence, the system has **relative degree two** over R^2 .

- Consider the same system with the different that

$$y = x_2$$

$$\dot{y} = \varepsilon \left[-x_1 + x_2 - \frac{1}{3}x_2^3 + u \right],$$

Hence, the system has **relative degree one** over R^2 .

Model and Lie Derivative

- Consider the n -dimensional, single-input-single-output system

$$\dot{x} = f(x) + g(x)u, \quad y = h(x)$$

where f , g , and h are sufficiently smooth in a domain D , $f: D \rightarrow R^n$ and $g: D \rightarrow R^n$ are called **vector fields** on D .

- The derivative of y is given by

$$\dot{y} = \frac{\partial h}{\partial x} [f(x) + g(x)u] \stackrel{\text{def}}{=} L_f h(x) + L_g h(x)u$$

Model and Lie Derivative-Cont'd

- Lie Derivative of h with respect to f or along f .

$$L_f h(x) = \frac{\partial h}{\partial x} f(x)$$

- This is the derivative of h along the trajectories of the system $\dot{x} = f(x)$.
- The new notion is convenient when we repeat the calculation of the derivative with respect to the same vector field or a new one. For example,

$$L_g L_f h(x) = \frac{\partial(L_f h)}{\partial x} g(x)$$

$$L_f^2 h(x) = L_f L_f h(x) = \frac{\partial(L_f h)}{\partial x} f(x)$$

$$L_f^k h(x) = L_f L_f^{k-1} h(x) = \frac{\partial(L_f^{k-1} h)}{\partial x} f(x)$$

Relative Degree

- The first derivative

$$\dot{y} = L_f h(x) + L_g h(x)u$$

$$L_g h(x) = 0 \quad \Rightarrow \quad \dot{y} = L_f h(x) \quad (\text{independent of } u)$$

- The second derivative

$$y^{(2)} = \frac{\partial(L_f h)}{\partial x} [f(x) + g(x)u] = L_f^2 h(x) + L_g L_f h(x)u$$

$$L_g L_f h(x) = 0 \quad \Rightarrow \quad y^{(2)} = L_f^2 h(x) \quad (\text{independent of } u)$$

- The third derivative

$$y^{(3)} = L_f^3 h(x) \quad (\text{independent of } u)$$

Relative Degree-Cont'd

- The ρ th derivative

$$L_g L_f^{i-1} h(x) = 0, \quad i = 1, 2, \dots, \rho - 1; \quad L_g L_f^{\rho-1} h(x) \neq 0$$

$$y^{(\rho)} = L_f^\rho h(x) + L_g L_f^{\rho-1} h(x)u$$

Definition (Relative Degree)

The system

$$\dot{x} = f(x) + g(x)u, \quad y = h(x)$$

has **relative degree** ρ , $1 \leq \rho \leq n$, in $\mathcal{R} \subset D$ if $\forall x \in \mathcal{R}$.

$$L_g L_f^{i-1} h(x) = 0, \quad i = 1, 2, \dots, \rho - 1; \quad L_g L_f^{\rho-1} h(x) \neq 0$$

Example for Calculating a Relative Degree

- Consider the system

$$\dot{x}_1 = x_2/\varepsilon, \quad \dot{x}_2 = \varepsilon \left[-x_1 + x_2 - \frac{1}{3}x_2^3 + u \right]$$

$$y = \frac{1}{2} (\varepsilon^2 x_1^2 + x_2^2)$$

- The derivative is given by

$$\dot{y} = \varepsilon^2 x_1 \dot{x}_1 + x_2 \dot{x}_2 = \varepsilon x_2^2 - (\varepsilon/3)x_2^4 + \varepsilon x_2 u$$

Hence, the system has relative degree one in $\{x_2 \neq 0\}$.

Exercise for Calculating a Relative Degree

- Find the relative degree for the following system

$$\dot{x}_1 = d_1(-x_1 - x_2x_3 + V_a) \quad d_1 > 0$$

$$\dot{x}_2 = d_2[-f_e(x_2) + u] \quad d_2 > 0$$

$$\dot{x}_3 = d_3(x_1x_2 - bx_3) \quad d_3 > 0$$

$$y = x_3$$

- The derivatives are given by

$$\dot{y} = \dot{x}_3 = d_3(x_1x_2 - bx_3)$$

$$\ddot{y} = d_3(x_1\dot{x}_2 + \dot{x}_1x_2 - b\dot{x}_3) = (\dots) + d_2d_3x_1u$$

The system has relative degree two in $\{x_1 \neq 0\}$.

Relative Degree of Transfer Functions

- Consider a linear system represented by the transfer function

$$H(s) = \frac{b_m s^m + b_{m-1} s^{m-1} + \dots + b_0}{s^n + a_{n-1} s^{n-1} + \dots + a_0} \stackrel{\text{def}}{=} \frac{N(s)}{D(s)}, \quad (m < n, b_m \neq 0)$$

Its relative degree is $m - n$. Does the definition coincide with the previous one?

- The state-space equations of the transfer function is given by

$$\dot{x} = Ax + Bu, \quad y = Cx$$

$$A = \begin{bmatrix} 0 & 1 & 0 & \dots & \dots & 0 \\ 0 & 0 & 1 & \dots & \dots & 0 \\ \vdots & & \ddots & & & \vdots \\ & & & \ddots & & \vdots \\ & & & & \ddots & \vdots \\ \vdots & & & & & 0 \\ 0 & & & & & 1 \\ -a_0 & -a_1 & \dots & \dots & -a_m & \dots & \dots & -a_{n-1} \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ \vdots \\ 0 \\ 1 \end{bmatrix}$$

$$C = [\quad b_0 \quad b_1 \quad \dots \quad \dots \quad b_m \quad 0 \quad \dots \quad 0 \quad]$$

Relative Degree of Transfer Functions-Cont'd

- $\dot{y} = CAx + CBu, \ddot{y} = CA^2x + CABu, \dots, y^{(i)} = CA^i x + CA^{i-1}Bu$
- CA^i is obtained by shifting the elements of C two positions to the right.

When $i = n - m - 1$, we have

$$CA^{n-m-1}B = b_m \neq 0$$

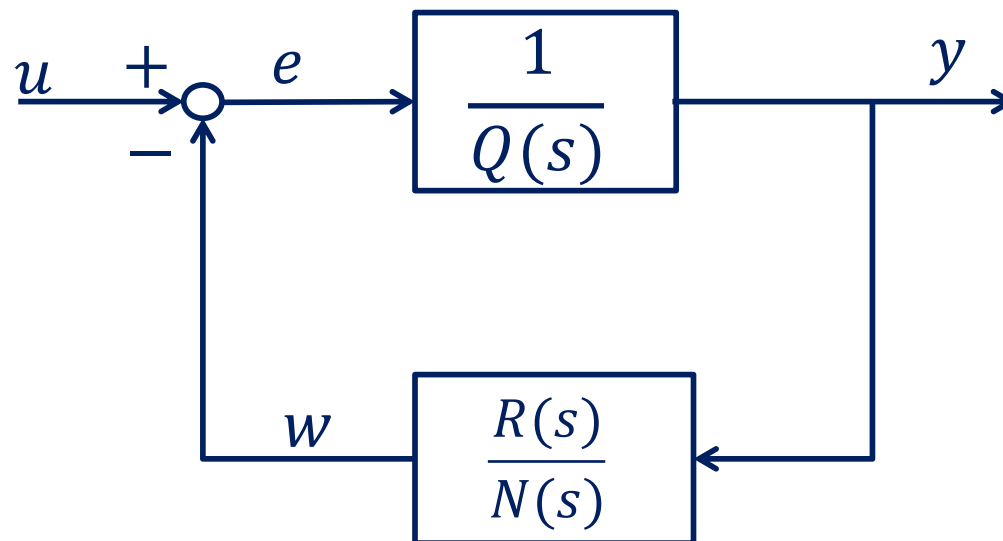
$$y^{(n-m)} = CA^{n-m}x + CA^{n-m-1}Bu \Rightarrow \rho = n - m$$

- These two definitions coincide!

Normal Form of Transfer Functions

- Let $D(s) = Q(s)N(s) + R(s)$, $Q(s), R(s)$ are the quotient and remainder polynomials, respectively. It follows that $\deg Q = n - m = \rho$, $\deg R < m$, the leading coefficient of $Q(s)$ is $1/b_m$.

$$H(s) = \frac{N(s)}{D(s)} = \frac{N(s)}{Q(s)N(s) + R(s)} = \frac{\frac{1}{Q(s)}}{1 + \frac{1}{Q(s)} \frac{R(s)}{N(s)}}$$



Normal Form of Transfer Functions-Cont'd

- State model of $1/Q(s)$: $\xi = \text{col}(y, \dot{y}, \dots, y^{(\rho-1)})$

$$\dot{\xi} = (A_c + B_c \lambda^T) \xi + B_c b_m e, \quad y = C_c \xi, \quad \lambda \in R^\rho$$

$$A_c = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & & \ddots & & \vdots \\ \vdots & & & & 0 & 1 \\ 0 & \dots & \dots & 0 & 0 \end{bmatrix}, \quad B_c = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix}, \quad C_c = [1 \quad 0 \quad \dots \quad 0 \quad 0]$$

Normal Form of Transfer Functions-Cont'd

- State model of $R(s)/N(s)$

$$\dot{\eta} = A_0\eta + B_0y, \quad w = C_0\eta$$

- Normal Form

$$\dot{\eta} = A_0\eta + B_0C_c\xi \quad \text{(internal model)}$$

$$\dot{\xi} = A_c\xi + B_c(\lambda^T\xi - b_mC_0\eta + b_mu) \quad \text{(external model)}$$

$$y = C_c\xi$$

The eigenvalues of A_0 are the zeros of $H(s)$.

- Can this idea be generalized to the following nonlinear system?

$$\dot{x} = f(x) + g(x)u, \quad y = h(x)$$

Example

- Consider the controlled van der Pol equation:

$$\dot{x}_1 = x_2/\varepsilon, \quad \dot{x}_2 = \varepsilon \left[-x_1 + x_2 - \frac{1}{3}x_2^3 + u \right], \quad y = x_2$$

$$\dot{y} = \dot{x}_2 = \varepsilon \left[-x_1 + x_2 - \frac{1}{3}x_2^3 + u \right] \Rightarrow \rho = 1$$

- The system is in the normal form with $\eta = x_1$ and $\xi = x_2$

$$y(t) \equiv 0 \Rightarrow x_2(t) \equiv 0 \Rightarrow \dot{x}_1 = 0$$

- How to choose the variables η and ξ ?

Normal Form of Nonlinear Systems

- Consider the system with relative degree ρ

$$\dot{x} = f(x) + g(x)u, \quad y = h(x)$$

- Find a change of variables $z = [\eta^T, \xi^T]^T$ such that the new state z can be partitioned into a ρ -dimensional vector ξ and $(n - \rho)$ -dimensional vector η , where η does not depend on u and y does not depend on η .

Normal Form of Nonlinear Systems-Cont'd

- The internal variables are defined as

$$z = T(x) = \begin{bmatrix} \phi_1(x) \\ \vdots \\ \phi_{n-\rho}(x) \\ \hline h(x) \\ \vdots \\ L_f^{\rho-1} h(x) \end{bmatrix} \stackrel{\text{def}}{=} \begin{bmatrix} \phi(x) \\ \hline \psi(x) \end{bmatrix} \stackrel{\text{def}}{=} \begin{bmatrix} \eta \\ \hline \xi \end{bmatrix}$$

- Choose $\phi(x)$ such that $T(x)$ is a diffeomorphism and

$$\frac{\partial \phi_i}{\partial x} g(x) = 0, \quad \text{for } 1 \leq i \leq n - \rho, \quad \forall x \in D_x$$

Normal Form of Nonlinear Systems-Cont'd

- The normal form is then given by

$$\dot{\eta} = \frac{\partial \phi}{\partial x} [f(x) + g(x)u] = f_0(\eta, \xi)$$

$$\dot{\xi}_i = \xi_{i+1}, \quad 1 \leq i \leq \rho - 1$$

$$\dot{\xi}_\rho = L_f^\rho h(x) + L_g L_f^{\rho-1} h(x)u$$

$$y = \xi_1$$

- The equation for ξ can be written as $\dot{\xi} = A_c \xi + B_c [L_f^\rho h(x) + L_g L_f^{\rho-1} h(x)u]$ and $y = C_c \xi$
- Does the transformation always exist?

Normal Form of Nonlinear Systems-Cont'd

Theorem

Suppose the system

$$\dot{x} = f(x) + g(x)u, \quad y = h(x)$$

has relative degree $\rho (\leq n)$ in \mathcal{R} . If $\rho = n$, then for every $x_0 \in \mathcal{R}$, a neighborhood N of x_0 exists such that the map $T(x) = \psi(x)$, restricted to N , is a diffeomorphism on N . If $\rho < n$, then, for every $x_0 \in \mathcal{R}$, a neighborhood N of x_0 and smooth functions $\phi_1(x), \dots, \phi_{n-\rho}(x)$ exist such that

$$\frac{\partial \phi_i}{\partial x} g(x) = 0, \quad \text{for } 1 \leq i \leq n - \rho$$

is satisfied for all $x \in N$ and the map $T(x) = \begin{bmatrix} \phi(x) \\ \psi(x) \end{bmatrix}$, restricted to N , is a diffeomorphism on N .

Zero Dynamics and Minimum Phase

- Consider the normal form

$$\dot{\eta} = f_0(\eta, \xi)$$

$$\dot{\xi} = A_c \xi + B_c \left[L_f^\rho h(x) + L_g L_f^{\rho-1} h(x) u \right]$$

$$y = C_c \xi$$

- When the output is identically zero, we have

$$y(t) \equiv 0 \Rightarrow \xi(t) \equiv 0 \Rightarrow \dot{\eta} = f_0(\eta, 0)$$

Definition

The equation $\dot{\eta} = f_0(\eta, 0)$ is called the **zero dynamics** of the system. The system is said to be **minimum phase** if the **zero dynamics have an asymptotically stable equilibrium point** in the domain of interest.

Exercise

- Consider the controlled van der Pol equation:

$$\dot{x}_1 = x_2/\varepsilon, \quad \dot{x}_2 = \varepsilon \left[-x_1 + x_2 - \frac{1}{3}x_2^3 + u \right], \quad y = x_2$$

$$\dot{y} = \dot{x}_2 = \varepsilon \left[-x_1 + x_2 - \frac{1}{3}x_2^3 + u \right] \Rightarrow \rho = 1$$

- Find the zero dynamics of the proposed system and see if it is minimum-phase?
- The system is in the normal form with $\eta = x_1$ and $\xi = x_2$

$$y(t) \equiv 0 \Rightarrow x_2(t) \equiv 0 \Rightarrow \dot{x}_1 = 0$$

No asymptotically stable equilibrium point, hence, non-minimum phase.